Factors effecting field emission from multiwalled carbon nanotubes

Abhilash Krishna

Louisiana State University and Agricultural and Mechanical College

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FACTORS EFFECTING FIELD EMISSION FROM MULTIWALLED CARBON NANOTUBES

A Thesis

Submitted to the Graduate Faculty of the Louisiana State University and Agricultural and Mechanical College in partial fulfillment of the requirements for the degree of Master of Science in Electrical Engineering

in

The Department of Electrical and Computer Engineering

by
Abhilash Krishna
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DEDICATION

To my parents and teachers for their love, encouragement & criticism.
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SYMBOLS AND CONVENTION USED

• $E$: Local Electric field
• $\gamma$: Field enhancement factor
• CNT: Carbon nanotube
• FE: Field Emission
• MWNT: Multi walled carbon nanotube
• SWNT: Single Walled Carbon nanotube
• $V_{on}$: Turn on voltage
• $V_{th}$: Threshold voltage
• $V_p$: Potential energy on an electron inside the metal
• $\phi$: Work function
• $e$: Charge of an electron
• $\zeta$: Fermi energy level
• $U$: Total energy of the electron
• $W$: $x$-part of the total energy
• $m_e$: mass of an electron
• $x$: distance from the emitter surface
• $P_x$: momentum of the electron in $x$-direction
• $J$: Field emission current density
• $I$: Field emission current
• $K$: Boltzmann constant
• $T$: Absolute temperature
• $h$: Planck’s constant
• $A$: Field emitting area in the first approximation
• $Z$: Atomic Number
• $E_{ion}$: Ionization Energy
• $\theta$: Scattering Angle
• $\Omega$: Solid Angle
• $\theta_0$: Screening Angle
• $c$: Velocity of light in vacuum
• $\lambda$: Wavelength
• $\nu$: Electron Velocity
• $E_{kin}$: Kinetic energy of an electron
ABSTRACT

Carbon nanotubes (CNT) have emerged to be one of the most versatile of materials ever discovered. The small dimensions, high electrical conductivity and strength along with other physical and electrical properties make them a unique material with a wide range of promising applications. One such use is that of CNTs as electron beam sources.

A typical CNT has a diameter of only a few nanometers but can be hundreds of microns long. Applying a voltage across the length of such an object results in field emission of electrons from one end of the tube. This effect is due to intense electric field enhancement that occurs at the ultra sharp tip of the nanotube. A viable field emission electron beam source can be fabricated from CNTs.

The primary goal of this work is to study the effects of various factors that influence field emission from multiwalled CNTs. For the set of factors that was chosen for investigation, a suitable field emission testing system was designed and assembled. Temperature of the CNTs was observed to have a considerable effect on the field emission from CNTs. Current saturation is observed at high temperatures. These findings can prove to be critical if the field emission device is operating in conditions of high temperature. The effects of variation in ambient pressure and changes in the background gas species are also studied. The field emission device characteristic is found to be very sensitive to the ambient gas pressure and more so when the gas species used was helium. Among Ar, He and N2, it is observed that He is the most suitable for field emission based device applications. It has been experimentally proven that aligned CNTs are far superior to random CNTs in terms of field emission characteristics. Effect of different substrate materials on field emission has also been examined. It has been found that metallic substrates like stainless steel show promise of better performance. CNT growth conditions have
also been shown to influence their field emission property. Young’s interference fringes found on the copper anode surface after field emission have been reported here. Emitter and anode degradation as a result of field emission have been discussed as part of this work. However it is important to note that CNTs are relatively more robust and less prone to degradation when compared to many other conventional field emitters. These results can be applied to find a set of optimal parameters that could be used for any field emission device design in order to get maximum field emitted current density at low operating voltages.
1. INTRODUCTION

Carbon nanotubes (CNTs) have many exceptional properties that make them attractive for a variety of applications. In particular, previous work has shown that CNTs can have outstanding electrical field emission properties, with high emission currents at low electric field strengths. CNTs are hence attractive as cold-cathode field emission sources, especially for applications requiring high current densities (hundreds to thousands of amperes per cm\(^2\)) and lightweight packages. Recently, there have been numerous fundamental works on optimization of field emission from CNTs. However, achieving high current densities over large sample areas of CNTs with repeatability and emission longevity still remains an open problem. This is mainly due to the fact that field emission from CNTs depends on a wide range of factors which span from conditions during the CNT growth to the conditions during the field emission operation. To comprehend how these various factors affect field emission, it is extremely crucial to understand the basic physics that governs field emission.

1.1 Background

- Principle governing field emission

Field emission is the extraction of electrons from a solid material by tunneling through the surface-potential barrier under the influence of a strong external electric field. The potential barrier is rectangular when no electric field is present, and becomes triangular when a negative potential is applied to the solid. The slope of the latter depends on the amplitude of the local electric field \(E\) just above the surface. This local electric field is drastically enhanced if the structure of the emitter is very sharp and protruding (High Aspect Ratio) as in the case of a CNT.
Fig. 1.1 Potential-energy diagram illustrating the effect of an external electric field on the energy barrier for electrons at a metal surface. \( V(x) \) is the one-dimensional potential energy of an electron as a function of its distance \( x \) (in Å) from the metal surface. \( \phi \) is the work function and \( V_p \) is the potential energy of the electron inside the metal. \( E \) is the local electric field at the surface [1].

- **Fowler-Nordheim Model**

  The Fowler-Nordheim Model [1] describing the electron emission from metals into a region of high electric field in vacuum is framed based on the following assumptions:

  1) The temperature of the metal is 0 °K.
  2) The free-electron approximation applies inside the metal.
  3) The surface is considered to be smooth (any irregularities that are present are negligible compared to the width of the potential barrier) and plane.
  4) The potential barrier close to the surface in the vacuum region consists of an image-force potential and a potential due to the applied external electric field.
The image force is a columbic force of attraction pulling the electron emitted towards the
surface due to its induced charge inside the metal. It can be observed from the Fig.1.1 that the net
potential energy of the electron is a result of the summation of the image force potential and the
potential due to the applied external electric field at the surface.

The potential energy of the electron can be given as:

For \( x < 0 \) as \( V(x) = V_p \) \( (1.1) \)

And for \( x > 0 \) as \( V(x) = \frac{-e^2}{4\pi \varepsilon x} - eEx \) \( (1.2) \)

Where \( e \) is the magnitude of charge of the electron and \( E \) the electric field strength. As \( V(x) = 0 \)
at the vacuum level the numerical values of Fermi level \( \zeta \) and \( V_p \) are negative. A discontinuity
occurs at the Metal-Vacuum boundary. The fowler Nordheim model for field emission is based
on tunneling of electrons through a one dimensional potential barrier as shown in the Fig.1.1.

\( U \) is the total energy of the electron and \( W \) is the \( x \)-component of the total energy.

\[
W = \frac{p_x^2}{2m_e} + V(x) \quad (1.3)
\]

\( p_x \) is the momentum of the electron in the \( x \)-direction and \( m_e \) is the mass of the electron.

In this model an assumption is made that only \( W \) determines the penetration probability of the
potential barrier by an electron.

The Fowler-Nordheim equation gives a relationship between the emission current
density \( J \), the electric field strength \( E \) and the work function \( \phi \). The supply function \( N(W)dw \)
equals the number of electrons with the \( x \)-component of their energy within the range \( W \) to
\( W + dw \) incident on the surface per unit area and time. This supply function is multiplied by the
energy dependant probability for barrier penetration \( D(W) \). The number of electrons \( P(W) \) in the
range $W$ to $W+dW$ tunneling from the metal into the vacuum region is usually called the normal energy distribution:

$$P(W)dW = N(W)D(W)dW \quad (1.4)$$

The Fowler-Nordheim Equation is found by integrating over all values of $W$:

$$J = e \int_{V_p}^{\infty} P(W)dW \quad (1.5)$$

Though it is true that electrons escape from the metal as a result of field emission it is assumed that the equilibrium of electrons inside the metal is not disturbed. The supply function is derived from the Fermi-Dirac energy distribution.

The probability for barrier penetration $D(W)$ is found by solving the Schrödinger equation, substituting for the potential energy $V(x)$ as given in (1.2). Wentzel-Kramer-Brillouin (WKB) approximation, valid only for the condition when the $x$-component of the total energy $W \ll V_{\text{max}}(x)$ is applied. $V_{\text{max}}(x)$ is the maximum potential energy of the electron in the vacuum region. It is assumed that all the electrons penetrating the barrier originate in the neighborhood of the Fermi level.

Integrating the normal energy distribution over all $W$ and multiplying by $A$ which represents in first approximation the emitting area (in $m^2$), expressing the current $I$ in Amperes, the electric field strength $E$ in V/m, the work function $\phi$ in eV and substituting the numerical values for all constants results in

$$I = A \frac{1.5 \times 10^{-6}}{\phi} E^2 \exp\left(\frac{10.4}{\sqrt{\phi}}\right) \exp\left(-\frac{6.44 \times 10^9 \phi^{1.5}}{E}\right) \quad (1.6)$$
For typical values encountered in carbon based emitters \((A = 10^{-12} \text{ to } 10^{-14} \text{ m}^2, \phi = 4.9 \pm 0.1 \text{ eV})\) tunneling through the surface barrier becomes significant for fields above \(~3 \text{ V/nm}\) [2]. Although the Fowler Nordheim model has been originally developed for flat metallic surfaces at 0 K, it has proven adaptable to describe field emission from carbon based electron emitters [3].

To reach the field of \(~3 \text{ V/nm}\) necessary to extract electrons, field emitting structures with high aspect ratio’s like sharp objects or protrusions on a surface are employed to amplify the electric field. In that case, the local electric field is not simply \(\frac{V}{d}\) the applied voltage, \(V\), divided by inter-electrode distance, \(d\) but is higher by a factor \(\gamma\), which gives the emitter the ability to enhance the field and is accordingly termed the field-enhancement factor. \(\gamma\) is a geometrical parameter that depends on the dimensions and shape of the emitter and on its surroundings, as well as on the shape and distance of the counter electrode. The Electric field \(E\) at the emitter surface is written as

\[
E = \frac{\mathcal{W}}{d} \quad (1.7)
\]

and (1.7) can be re-written as

\[
I = A \frac{1.5 \times 10^{-6}}{\phi} \left(\frac{V}{d}\right)^2 \gamma^2 \exp\left(\frac{10.4}{\sqrt{\phi}}\right) \exp\left(-6.44 \times 10^9 \phi^2 \frac{d^3}{\mathcal{W}}\right) \quad (1.8)
\]

\(\gamma\) is an important parameter for field emission and can be extracted from the Fowler Nordheim plot, where \(\ln(I/V^2)\) is plotted against \(1/V\). Alternatively, \(\gamma\) can be estimated from the geometry: for nanotubes the models developed for a cylinder of height \(h\) terminated by a half sphere of radius \(r\) on a flat surface can be used, which states that

\[
\gamma = 0.7 \times \frac{h}{r} \quad (1.9)
\]
When \( h \) is far smaller than the interelectrode distance \( d \).

Equation 1.8 shows quantitatively how the field emitted current depends on the applied voltage, work function of the emitter and the field enhancement factor. These parameters in turn depend on various conditions like the temperature of the CNT, the ambient pressure of operation, orientation of CNT (random vs aligned), type of gas environment and many other factors.

1.2 Literature Review: Factors that Affect Field Emission from CNTs

Numerous fundamental works have been carried out to optimize field emission from CNTs by getting a handle over the various factors that influence it. Hence, before beginning experimental studies a detailed review of the past work was carried out. An overview of the various factors that influence field emission from CNTs is outlined here.

1.2.1 Temperature of the CNT

It has been observed by various groups [4,5] that field emission of electrons from metals like tungsten strongly depend on temperature especially at high temperatures. It has been reported that at high temperatures a combined effect of field emission as well thermionic emission results in the net measured current [4]. Dolan et al. reported a change in work function as a result of a rise in emitter temperature. As observed earlier from Equation 1.8 any change in the work function of CNTs would translate into a significant change in the field emitted current. Increased temperature could have an effect on the electrical conductivity of the CNTs depending on the type of CNTs used. The conductivity of a metallic CNT would decrease as a result of increased carrier scattering whereas the conductivity of a semi conducting CNT would get enhanced as a result of more temperature induced carrier generation. This conductivity modulation could affect field emission. A negative temperature dependent resistance in multi walled carbon nanotubes (MWNT) has been reported by Peng et al [6]. However if the transport
mechanism in the CNT as claimed by some groups [7] is quasi-ballistic then this conductivity
modulation should have minimal affect on field emission characteristics.

The temperature of the CNT is bound to increase as a result of resistive joule heating
during field emission. This being so if the CNTs are forcefully heated this might result in
lowering of the temperature gradient between the CNT base and tip thus minimizing thermally
induced stress gradient which in turn might improve the CNT field emitter lifetime.

The data in Fig.1.2 reported by a group studying growth of CNT characterized by field
emission measurements during CVD [8] shows that there is a definite effect of the CNT
temperature on its field emission characteristics. The CNT grown in this case was a mixture of
both metallic as well as semi-conducting types. Hence experiments were carried out as part of
this thesis work to understand the temperature dependence of field emission from MWNTs.

![Fig. 1.2 Emitted current versus time (I-t) for an applied voltage of 3 kV during a heating-cooling
cycle of 0 to 700 °C all other conditions remaining the same. From reference [8] with permission
(Appendix: C1).](image)

1.2.2 Ambient Pressure of the Surrounding Gas During Field Emission

The field emission spots were found to be sensitive to adsorbed gas molecules. This
caused an emission change of the particular site where the gas atom was adsorbed [9]. The
number of the gas molecules adsorbed depends not only on the emitter surface area but also on the background ambient pressure of the gas.

Depending on the type of gas the emission change after adsorption may be reversible after heat treatment of the CNTs. The temperature of the CNT rises as a result of prolonged field emission which may cause the adsorbed molecules to leave its surface depending on the type of gas molecule adsorbed.

This phenomenon in-turn influences the uniformity and stability of emission. This process of alteration of the field emission characteristic due to adsorption and desorption of gas molecules is attributed to the variation of energy barrier height for field emission at the gas adsorbed site.

The images shown in fig 1.3 were observed during field emission from a multi walled carbon nanotube. The images formed on a phosphor screen were recorded in this case using a CCD camera. It is believed that the adsorbents will be driven to the cap by the field and will alter the localized state. This not only causes a change in the intensity of the emission but also alters the geometry of the image obtained. This can be very clearly observed from the Fig. 1.3

This shows the dynamic nature of the surface near the tip of the CNT due to the adsorbed molecules. The intensity of the field emission spots were observed in this case in an Ultra high vacuum system with a pressure of $1.8 \times 10^{-8}$ mbars. It was observed that a clear nanotube emits a pattern containing pentagons or hexagons. The presence of an adsorbed molecule distorts this regularity.
Another noteworthy phenomenon that was observed by a group that conducted real-time measurement of pressure inside field-emission displays was that the sealed pressure inside the display cavity rapidly decreased owing to prolonged field emission which was quite similar to ion-pumping effects observed in other vacuum electron tubes [10]. Figure 1.4 shows the decrease in pressure measured with a spinning rotor gauge.

The ion pumping effect observed could be a reason for the current saturation observed with increasing emitter current. Thus this forces one to think that high ambient
pressure is detrimental to the high current operation of the field emitter because the ion pumping effect is pronounced in this operation regime.

Fig. 1.4 Direct observation of the ion pumping effect in a sealed field emission display. As soon as the device is turned on, the package pressure drops rapidly. From reference [10] with permission (Appendix: C2).

In this thesis work, field emission experiments were hence carried out at various ambient pressures of operation to identify the nature of dependence of the field emitted current density on the background pressure. It is extremely important to optimize this factor in order to boost the field emitted current.

1.2.3 Type of Ambient Gas Environment

One of the main concerns of a field emission based device is to reduce the operating voltage. One way to achieve this is to introduce suitable adsorbates that might effectively lower the ionization potential (IP) and facilitate the extraction of electrons. Recent experiments indicated that water molecules adsorbed on CNT tips significantly enhance field-emission current. However, a gradual decrease of field enhancement was found on single wall nanotubes when a partial pressure of O₂ was introduced in the chamber [11].
Unlike water molecules the presence of oxygen and hydrogen did not appreciably affect the field emission behavior. It is believed water gets attracted to metallic nanotube tips under field-emission conditions, and forms complexes that are stable at several hundred degrees above room temperature [12]. Resulting electrostatic interactions from the adsorbates make the highest occupied molecular orbital (HOMO) level in the nanotube more unstable, with a corresponding decrease in the ionization potential. The instability of the HOMO and the lowering of IP are both enhanced with an increasing number of water molecules adsorbed (up to a saturation density). H₂ weakly interacts with the nanotube tip even under field-emission conditions, and is not stable at room temperatures [12]. As part of this work three gas species He, N₂ & Ar were selected to be used to see if they caused any enhancement in the field emitted current.

1.2.4 Type, Alignment, Inter-tube Spacing, Cap-structure and Geometry of the CNTs

- Type of Carbon Nanotubes (SWNT/MWNT)

SWNT generally have a smaller diameter and higher degree of structural perfection than MWNTs, and thus SWNTs have the capability of achieving higher current densities and a longer life time [13]. The diameter of the SWNTs is usually in the range of 1–2 nm while the diameter of the MWNTs is 20–100 nm. This suggests that the SWNTs have a very high aspect ratio.

This however does not directly translate itself into a very high electric field amplification factor. The reason for this is that they normally form close-packed bundles comprising 10 to 100 SWNTs with a bundle diameter of 10–100 nm. Hence the effective bundle diameter decides the field amplification factor of these emitting structures. It can be seen from Fig 1.5 that the field emission characteristics of SWNT exhibits lower turn-on voltage when compared to the MWNT.
Alignment/Orientation of Carbon Nanotubes

From ultraviolet photoelectron spectroscopy (UPS) measurement, the aligned MWNTs were found to have a larger density of states at the Fermi level and a slightly lower work function than the random MWNTs which is attributed to the difference in the electronic state between the tip and the sidewall of the CNT [14]. Because the electrons are emitted from the tips of the CNTs, intuitively one would expect that the vertically aligned CNTs are better emitters than the random films. However this issue is complicated by the effect of electrical screening. Most of the vertically aligned MWNTs fabricated by chemical vapor deposition (CVD) process comprise densely packed CNTs. As a result they do not show enhanced emission properties as expected due to the Electrical screening effect. It can be observed from Fig 1.7 that the higher the potential gradient the higher is the electric field at the tip of the CNT emitter. The presence of neighboring CNTs very close to it greatly reduces this potential gradient by not allowing the equi-potential line to form a concave shape facing downwards with a very small acute angle.
As shown in Figure 1.5, the emission characteristic of the aligned MWNTs is significantly different from that of the random MWNT film. By lithographically patterning the location of the catalysts on the substrates, several groups have recently reported aligned CNTs and carbon nanofibers with controlled spacing to minimize the screening effects. One concern of this approach is whether the lifetime of the cathode is affected because of the significant reduction in the density of the CNTs. For cathodes with randomly oriented CNTs, the emitters come from two sources. One is the small fraction of the CNTs that point to the current collector due to simple statistical distribution. The second group comes from field induced alignment. Several experiments [15,16] have shown the CNTs can be easily bent and aligned to the electrical field direction under a moderate electrical field. One advantage of this type of cathode is the large number of CNTs available for emission which can lead to a longer lifetime.

Since lifetime as well as high current extraction are critical factors in deciding the acceptability of a CNT field emitter, according to our plan, experiments were carried out to compare a random and a well aligned CNT sample with the same physical layout to see how orientation affects the field emission current.

- **Inter-tube Spacing**

  When very short CNTs are grown (~ 5 micron range) there is some height variation between nanotubes that causes the longer nanotubes to be more emissive than the shorter ones nearby thus artificially reducing the density of the emitters. As explained earlier the electrical screening effect is detrimental to the field emission from CNTs. Calculations have shown that to minimize the screening effect the individual emitters/CNT should be evenly separated such that their spacing is greater than their height [13]. This would help in exploiting the very high current carrying potential of the CNTs.
Fig. 1.6 Schematics illustrating the different geometries of macroscopic CNT field emission cathodes and images of the actual CNT structures fabricated. In the ideal case (top), the CNTs are aligned in the field direction and well-spaced (S/H > 1) so that there is less electrical screening. From reference [13] with permission (Appendix: C4).

- **Structure of the Cap**

  A theoretical study predicted that an open-ended SWNT has much better field-emission properties than a closed SWNT [13], due to the electronic effects that alter the bonding mode and decrease the work function. No experiments have been reported yet on the comparison of open and closed SWNTs. In the case of a closed-capped MWNTs simulation results showed that the emission current drastically increases with a small increase in the major radius of the ellipsoidal tip. For open-ended MWNTs with flat top and round edges the emission current is observed to depend highly on the sharpness of the edges. The simulation results show that the emission
current mostly comes from the outer corner of the flat top and both inner corner and the flat top plays very little role in the filed emission process [13].

- **Structure and geometry of the carbon nanotube**

  The geometry of the CNT has a direct impact on its field emission properties. Experimental results show that the emission threshold field increases with decreasing CNT bundle length $L$ as shown in fig.1.7(c). Keeping the diameter of the CNT constant, the lengthening of the nanotubes which causes an increase in its aspect ratio is observed to provoke an increase of the emitted current at constant applied voltage because of the increase in the field enhancement factor.

  Fig 1.7(a, b) clearly shows the field enhancement occurring at the tip of the CNT emitter due to its favorable aspect ratio. It can be observed from the figure that the electric field which is given by the rate of change of the voltage with distance $dV/dx$ is maximum near the surface of the emitter. The anomaly observed in Fig1.7(c) when the length of the CNT goes from 5 um to 13 um reiterates the fact that for a given CNT emitter density there is an optimum CNT length to CNT spacing ratio required to get maximum field emitted current per cm$^2$ all other conditions remaining the same.

  The field emission characteristic is also found to be dependant on the chirality [18] of a CNT. The chirality of the CNT in turn decides the metallic or the semiconducting nature of the CNT. A metallic tube has a line density ($j_L$) higher than that of a semiconducting one. The line density is defined as the current per unit length of the CNT under test. Also, for semiconducting tubes, a tube of larger chiral angle has a line density higher than that of smaller chiral angle; a zigzag semiconducting tube has a smallest line density among the others. These facts can be noted from Fig. 1.8.
Fig. 1.7 Sketch of an anode 10 um above a carbon nanotube showing field enhancement at the electrode surfaces. The potential distribution is given in (a) with each band denoting 5 V potential change. The voltage distribution in the gap is given in (b) with the corresponding field distribution in the inset. (c) results showing decreasing emission threshold field with increasing CNT bundle length L. From reference [17,4] with permission (Appendix: C5, C6).
Fig. 1.8 (a) The line density versus the field strength (jL–F) characteristics of four typical SWNTs. The zigzag (12, 0) and chiral (12, 3) SWNTs are metallic and the chiral (12, 1) and (12, 10) SWNTs are semi conducting. The line densities of currents vs. the chiral vector Ch= (12, m) of SWNTs from m=0 to m=12 are also shown in the inset. (b) The FN plots for the four SWNTs and their derivative sFN =d ln (jL /F2)/d (1/F) (inset). From reference[18] with permission (Appendix: C7).

1.2.5 Type of Substrate Material Used for CNT Growth

Different substrate/base materials on which the CNT is grown would have different values of resistivity hence would result in different electric field threshold voltages. Nanotubes can be self doped by the material of the substrate on which it is grown [19]. This would also affect its field emission characteristics. Hence, a careful study of the dependence of field emission from CNTs on the substrate material becomes imperative. Different substrate materials like SiO₂, nickel & stainless steel have been tested for field emission.

1.2.6 Conditions During CNT Growth

CNTs can be fabricated in laboratory quantities by several techniques including arc-discharge, laser ablation and chemical vapor deposition (CVD) [20]. The structure and morphology of the CNTs fabricated by each technique vary significantly. The arc-discharge and
laser-ablation methods use extremely high temperatures – the temperature of the plasma/plume is 3000–4000 °C. As a result the CNTs produced tend to have a higher degree of graphitization than those produced by the CVD process which normally operates at 800–1200 °C. The defect density affects the thermal and electrical conductivity, the mechanical strength of the CNTs and therefore their emission characteristics due to stable CNT heating and subsequent destruction during field emission.

A study revealed more flickering and instability in the field emission from microwave plasma enhanced CVD (MPECVD) grown CNTs when compared to thermal CVD grown CNTs which is due to the excessive catalytic metal particles present inside and top of the MPECVD grown specimens[21]. The difference in uniformity in field emission from CNTs grown using these two processes can be seen from Fig.1.9.

Fig. 1.9 (a) Emission pattern of MPECVD-grown FEA with 20 mA at 4.1 V/mm. (b) Rise and fall sweeps of the MPECVD-grown CNT–FEA are not obtained due to the vacuum breakdown. (c) Uniform emission pattern of the thermal CVD-grown CNT–FEA with 2 mA at 4.25 V/mm. (d) Rise and fall sweeps of the thermal CVD FEA show lower turn-on voltage than that of MPECVD-grown CNT–FEA. From reference [21] with permission (Appendix: C8).
Metal particles are very harmful to dependable operation of the field emission array (FEA) because the melting and evaporation of metal particles by high emission currents abruptly surge the emission currents and result in vacuum breakdown, followed by the failure of the CNT–FEA. As part of this work, CNT growth was carried out under normal atmospheric pressure and in vacuum to compare field emission characteristics in both the cases.

The following factors discussed in sections 1.2.7, 1.2.8, 1.2.9 and 1.2.10 are found to affect field emission characteristics of CNTs. However their study is beyond the scope of this work. It has been included here to give the reader a complete picture.

### 1.2.7 Device Configuration

The device configuration decides the collection efficiency of the emitted electrons hence is a crucial factor to be noted during field emission device design. Due to the strong electric field enhancement of the edge, trajectory of the emitted electrons is deviated from the center of the electrode as shown in Fig. 1.10 (c) [22]. The electron deviation could be overcome if a gate electrode is incorporated between cathode and anode. This forces the need for a triode type of configuration which facilitates better focusing of the emitted electrons.

Recently a lot of work has been done in designing optimized triode type structures for assisting electron extraction as shown in Fig. 1.10 (b) however these types of designs suffered from high leakage currents as a result of the third accelerating electrode.

Having the luxury of a large collector in the sandwiched device structure used for this work the need for a third focusing electrode is avoided. Hence, a diode type of structure as shown in Fig. 1.10 (a) is used without compromising on the collector efficiency. This work also lays a foundation for the realization of a field emission based CNT diode that can be operated in both forward as well as reverse bias.
1.2.8 Source Used for CNT Synthesis

The field emission characteristic of CNT synthesized using different sources is observed to vary based on the source used. This has been experimentally verified. The results originally published by Materials Research Laboratories, Industrial Technology Research Institute, Hsinchu, Taiwan, R.O.C. [23] are summarized here.
Table 1.1 The experimental parameters for CNT synthesized by arc discharge method
From reference [23] with permission (Appendix: C3).

<table>
<thead>
<tr>
<th>Group</th>
<th>Specimen</th>
<th>Materials</th>
<th>Experimental Parameters</th>
</tr>
</thead>
<tbody>
<tr>
<td>G</td>
<td>G-1</td>
<td>graphite</td>
<td>He: 300mm Hg flow rate: 5 l/min reaction time: 5min</td>
</tr>
<tr>
<td>Ni/G</td>
<td>Ni/G-1</td>
<td>graphite + 5% wt. Ni powder</td>
<td>He: 300–500 mm Hg flow rate: 5–10 l/min reaction time: 10–15min</td>
</tr>
<tr>
<td></td>
<td>Ni/G-2</td>
<td></td>
<td></td>
</tr>
<tr>
<td>PAH/G</td>
<td>PAH/G-1</td>
<td>Graphite + pyrene coating</td>
<td>He: 300–500 mm Hg flow rate: 5–10 l/min reaction time: 2–3min</td>
</tr>
<tr>
<td></td>
<td>PAH/G-2</td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

The field emission characteristics measured for each specimen showed a clear distinction based on the source used for synthesis. A clear understanding of the cause is required to come up with the best source that can be used for growth in order to yield optimum field emission results. It can be deduced from Fig 1.11 that PAH/G-2 gives the lowest electric field threshold voltage and hence the best emission response.

Fig. 1.11 Field emission characteristics of CNT specimens. From reference [23] with permission (Appendix C2).
1.2.9 Surface Treatment – Gas Exposure

Gas exposure induces chemi- and physisorption of gas molecules on the surface of CNTs. As a result of surface treatment the presence of adsorbates is observed to enhance field emission at low fields and high vacuum conditions [21]. Increasing the field beyond a certain limit displaces the adsorbates (leading to fluctuations in emission current) and finally removes them. I-V curves acquired immediately after such a cleaning process is carried out shows higher onset fields.

Experimental study of the dependence of field emission on gas exposures of CNTs have been reported by a group which used oxygen, nitrogen and hydrogen for surface treatment of CNT before carrying out field emission experiments [21]. The results obtained are summarized below in Fig.1.12.

![Fig. 1.12 The F–N plots in terms of different gas species and exposure times. The F–N plots with the rise and fall sweeps for (a) N2, (b) O2, and (c) H2 show the hysteresis. From reference [21] with permission (Appendix: C8).](image)

In the rise bias sweep, the current saturation, indicated by arrows in Fig. 1.12, was observed and this resulted in two slopes. The current saturation occurred for all gases. A change in slope of the field emission characteristic due to saturation reflects in the Fowler Nordheim plot as well which can be seen from the Fig.1.12 The fall bias sweep initially showed only a single
slope; in other words, no current saturation. However, after long exposures of oxygen and nitrogen, current saturations indicated by arrows in Figs. 1.12(a) and 1.12(b) are observed even in the fall sweep, whereas the degree of saturation in the fall sweep is stronger in oxygen. However, shown in Fig. 1.12(c), the current saturation in the fall sweep after long hydrogen gas exposure did not occur, and additionally, the degree of hysteresis was reduced in hydrogen exposure. This result implied that the role of hydrogen gas is different from oxygen and nitrogen gases. It is manifested by the shift of F–N plots after each gas exposure. Oxygen and nitrogen exposures push the F–N plots toward the high voltage region, whereas hydrogen exposures pull them back to the lower-voltage region.

It is argued that similar tendencies in degradation of the emission properties resulting from oxygen and nitrogen exposures may be explained by the electronegativity and adsorption property of gases. Adsorption of materials with high electronegativity is said to hinder the electron emission by intensifying the local potential barriers [21].

It is believed that hydrogen gas removes adsorbates by bombarding the emitter surface with energetic hydrogen atoms, which consequently cleans the emitters. Therefore, the current saturation during the fall sweep at large gas-exposure times from oxygen and nitrogen gases is not observed from the hydrogen gas exposures. Therefore, hydrogenation of the CNT– FEA has the technical significance for the activation of the field-emission display, whose performance is degraded due to other adsorbates. Whereas, oxygen gas is believed to depress the field emission severely and even change the tip morphology by possible oxidative etching [21].

1.2.10 Doping

As is the case of other carbon allotropes, the electronic properties of the CNTs can be modified and tuned by chemical doping. Experimentally, it has been shown that the work
function of the SWNTs can be reduced to as low as 2.5 eV by intercalation with Cs [13]. Each alkali metal atom can donate one electron to the SWNT which results in the reduction of the work function. A recent theoretical calculation shows the same trend as the experimental result [2]. The effect of Cs intercalation on the field emission properties has also been studied. The result showed that Cs deposition on SWNTs can decrease the turn-on field by a factor of 2–3 and increase the emission current [13], consistent with reduction of the electronic work function due to Cs intercalation. The intercalated CNTs however are air-sensitive and can easily de-intercalate when the emission current is high.

As explained earlier nanotubes can be self-doped by material of substrate [17]. It is known that the dopants can have different localization in the MWNT giving different distributions lengthwise in the nanotube. The dopant site can be in the enclosure of MWNT such as between their walls or on the surface etc. This could change the electronic structure of nanotubes and in turn have a consequence on their field emission properties.

To achieve the goal of maximizing the current density at lowest possible threshold voltage it is necessary to investigate the nature of dependence of the field emitted current over the various factors discussed here. This need for a detailed study determined the scope of work carried out as part of this thesis.

1.3 Scope of Work

The spectrum of work that was intended to be carried out and that has been successfully completed is illustrated in a sequential fashion in Fig. 1.13. The work began with the analysis of experimental requirements which was followed by the stage of system design and assembly. On a parallel track Microfabrication and CNT synthesis and treatment was carried out. This was followed by experimentation. During experimentation problems with manual data recording
forced the need for system automation and control using Labview 7.0. This thesis mainly focuses on investigation of the dependence of field emission from multi-walled CNTs on the temperature of the CNT sample, the pressure of operation, the orientation of the CNTs & the ambient gas environment and the substrate used for growth.

The work also discusses how the CNT emitter degrades as a result of repeated runs of field emission experiments. In this work, a multi-purpose experimental system is designed and assembled in order to accurately control the various variable parameters that influence field emission. The automation of the experimental system was carried out using the Labview 7.0 software enabling dynamic data acquisition & generation of Fowler-Nordheim plots as the field emission experiment progresses. UV photolithography is used for opening up windows in Chromium/Gold layer exposing the underlying SiO$_2$. This was carried out by selectively etching Cr/Au that was deposited on top of SiO$_2$. The windows of SiO$_2$ thus formed were used to selectively grow multi-walled CNTs in a horizontal thermal CVD furnace. Characterization of the MWCNT grown was carried out using SEM & TEM. Different types of test fixtures have

Fig. 1.13 Schematic showing scope of work involved in this thesis
been used for field emission in order to zero down on the most efficient one in terms of life time and the obtained field emission current density. Enhancements in the experimental system designed have been suggested in detail. Among various novel applications pointed out the use of CNTs as a field emission based diode has been experimentally verified. The main objective is to determine a set of conditions/parameters that would result in maximum field emission current density at the lowest possible applied electric field causing least damage to the CNT emitter thus increasing its lifetime.

1.4 Organization of Thesis

In chapter 1, relevant concepts in theoretical physics governing field emission have been covered. The Fowler Nordheim model is discussed in detail leading to the derivation of the Fowler Nordheim equation. The field emission analysis is initially carried out for the case of a metal emitter and extrapolated to the case of a CNT. The overall scope of this thesis is discussed. Various factors that affect field emission from CNTs have been highlighted.

In chapter 2 the system that was designed and assembled to carry out field emission experiments is discussed in detail. Its capabilities and drawbacks are discussed. Details of the program written for dynamic data acquisition and generation of Fowler-Nordheim plots are covered.

In chapter 3 the different approaches of microfabrication employed are presented. The reason for the approach adopted is explained. An overview of the process of CNT synthesis that is used is discussed. The structure and characteristics of CNT grown as obtained from TEM and SEM are covered.

In chapter 4 results of various experiments performed are presented. The effect of temperature, pressure, different ambient gases & physical layout on field emission from CNTs is
discussed in detail. The various observations made during experimentation are highlighted with evidence.

In chapter 5 recommendations for further research are given and conclusions are drawn. Prospects and limitations of MWNT as a field emission source are discussed. Enhancements to the current experimental system are submitted. Novel areas of application to CNT field emission sources are presented. Symbols & conventions used are enlisted on page x.
2. EXPERIMENTAL SYSTEM DESIGN AND AUTOMATION

2.1 Overview of the System

The experiments that dictated the design of the field emission system are

1. Recording field emission current from MWNTs as the voltage is incremented in steps from 0 to 5000 V.

2. Measurement of field emission current with varying temperature of the CNT samples.

3. Investigation of the dependence of field emission current on the ambient pressure of operation.

4. Study of the impact of various gases like He, N$_2$ & Ar on field emission from MWNTs.

A high voltage supply that could source any voltage between 0V to 5000 V was required to be applied across the length of MWNTs to force electrons to be field emitted. Keithley Model 248 high voltage supply was used for this purpose. This had the advantage of possessing a GPIB interface that could be used to remotely control it.

The turn-on voltage of a CNT field emitter is defined as the applied voltage for which the field emission current density is equal to 10uA/cm$^2$. The typical effective field emitting area could be as small as 10$^{-6}$cm$^2$. (a square island with a side of length 10um). Hence to determine the turn on voltage of such a field emitting structure a Pico-ammeter was necessary. Keithley 6485 pico-ammeter was used for this purpose. This model also had a GPIB interface for remote control. The range of measurable current using this instrument is 2nA to 20mA. The resolution of the reading from the pico-ammeter is of the order of femto-ampere however owing to the noise level, measurements below nano-ampere could not be achieved.

The second study required a stage whose temperature could be remotely controlled. The capability desired was to precisely control sub-zero to very high temperatures. A custom designed stage was built in order to facilitate these temperature dependant measurements. The design had two stages S1 and S2. S1 could be used to reduce the sample temperature to $-193^\circ$C.
S2 could be used to heat the sample up to 1600°C. The stage S1 which is a brazed copper reservoir achieves low temperatures using liquid nitrogen. The stage S2 which is a 2° BN coated graphite heater stage achieves high temperature using a resistively heated coil. A programmable temperature controller allows setting the temperature of both the stages.

The third study forced the need for precise control & monitoring of pressure over a wide range. This was achieved by using three pressure gauges, an MKS Baratron capacitance manometer with a range of $10^{-2}$T to $10^{-3}$T, a Granville-Phillips Convectron gauge with a range of $10^{-4}$T to 1 atm and a Kurt J Lesker Bayard Alpert Ion gauge with a range of $10^{-4}$T to $10^{-9}$T. A rotary vane mechanical pump in conjunction with an ion pump is used to pump down the vacuum chamber. The vacuum could be drawn to as low as $10^{-7}$T. An MKS Mass Flow Controller is used to adjust the flow of gas into the chamber in order to stabilize the pressure of the gas in the vacuum chamber at a specific desired value as the vacuum pump is left to run continuously. A multi-gauge controller is used to monitor pressure readings from all the three gauges.

To carry out the fourth function of the experimental system the vacuum chamber is provided with an inlet for gas. The desired gas is fed into the vacuum chamber from the respective cylinder through the Mass Flow Controller as explained earlier.

**2.2 Design of the System**

The Figure 2.1 shows the detailed design of the field emission experimental system highlighting the various inter-connections. Essentially the high voltage supply, the Pico-ammeter and the field emission test fixture placed inside the vacuum chamber are connected in series. Ceramic cased power feed-through is used to carry the high voltage from the power supply into the chamber. A PC is used for data acquisition from, and control of the high voltage supply and
the pico-ammeter. The mass flow controller is placed in between the gas cylinder and the vacuum chamber to regulate the pressure inside the chamber. The temperature controller can be programmed in advance to raise the temperature of the stage S1 in as low as steps of 5°C.

Fig. 2. 1 Design of the field emission experimental system.

Table 2.1 gives a brief summary of the various capabilities achieved by this system.

Although only Nitrogen and Helium (re-calibration was required) have been used other gases could be used as well provided the pressure gauges are calibrated accordingly.

Table 2.1 System Capabilities

<table>
<thead>
<tr>
<th>System Capabilities</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>Voltage Range allowed</td>
<td>-5000V to 5000V</td>
</tr>
<tr>
<td>Measurable current range</td>
<td>2nA to 20mA</td>
</tr>
<tr>
<td>Temperature range allowed</td>
<td>-193°C to 1600°C</td>
</tr>
<tr>
<td>Pressure range allowed</td>
<td>10⁻⁹ T to 1atm.</td>
</tr>
<tr>
<td>Types of gases that could be used</td>
<td>He, Ar, N₂</td>
</tr>
</tbody>
</table>

There is a scope for improving the system design to minimize the background noise level inorder to exploit the ultra low current measuring ability of the Keithley 6485 pico-ammeter. Measurement at sub-zero temperatures is also expected to bring down the noise level.
The experimental set up shown in figure 2.2 that was designed and assembled at the Center for Advanced Microstructures and Devices is totally functional.

Fig. 2.2 Experimental set up.

2.3 Safety Measures Incorporated

A protective circuitry is used to ensure that the pico-ammeter is safe in case the electrodes inside the vacuum chamber get shorted [24]. Keeping the 2002 National Electrical Code the entire circuit was designed giving utmost priority to personnel safety. Care has also been taken to avoid any damage to the equipment being used. This was very important considering the fact that the experiments performed require operation at high voltage and reasonably high currents.
Fig. 2.3 Two back to back diodes and a series resistor used to protect the pico-ammeter [24]

Levels of personnel safety incorporated:

- A circuit breaker is incorporated in the system design which would open up in case a current > 5mA is detected.
- 8 Gauge wires are used to ground individual equipments and the vacuum chamber to a common ground terminal.
- An algorithm for safety has been incorporated in the software during automation. This would instantaneously drop the voltage applied to zero in case a peak in current is detected.
- Every experiment is preceded by a safety inspection of the entire circuit.
- The front panels of the equipments are disabled during remote control from a PC while the experiment is going on. A safety switch is available to get back to local control.

2.4 Automation Using Labview 7.0

The high voltage supply and the pico-ammeter have a GPIB interface. This was made use of, in order to program using Labview 7.0 enabling automation of the entire experimental procedure including data acquisition and analysis. This was very essential considering the fact that loss of critical data points would render the experimental data acquired meaningless.
The tasks that have been achieved using Labview 7.0 are

1. Automatic equipment initialization, control & time synchronization.

The first step carried out by the program shown in Fig. 2.4 is to initialize the high voltage supply and the pico-ammeter. It then configures them for remote access and takes control of setting a voltage on the power supply and sensing the current from the pico-ammeter. This is done sequentially without causing any time conflicts between the instruments. Time synchronization is extremely crucial and is done in a way to maximize the speed of data acquisition.

![Fig. 2.4 The graphical program written for system automation](image)

2. Data acquisition.

The program shown in Fig. 2.4 executes in a loop incrementing the applied voltage by a user defined value followed by measuring the field emission current in a sequential manner using a time delay between iterations. These iterations are repeated until a set maximum voltage is
reached. The data obtained in each iteration is written onto a data file in pairs of voltage and current which can be used later.


In case the CNT field emitter sample inside the chamber is destroyed and both the electrodes get shorted in the middle of the experiment the system would continue to acquire data. It would result in loss of time if there was no direct way of knowing about such an event. Hence it became important to know the nature of the data getting generated as the experiment progresses. It was also important to know if the data generated was following the Fowler-Nordheim equation.

Hence a user interface as shown in Fig. 2.5 was created for the dynamic run-time plots in order to graphically see the progress of the experiment which could then be stopped in case of any mishap that occurs. Two important plots namely the current versus voltage curve and the Fowler-Nordheim curve are drawn and refreshed for every new data set being acquired.
Fig. 2.5 Labview User Interface showing the plot of current ($I$) versus Voltage ($V$) and also the Fowler-Nordheim plot drawn for $\ln(I/V^2)$ versus $(1/V)$.

4. Data Analysis

The generation of Fowler-Nordheim plot involves run-time data analysis. Labview 7.0 enables the use of mathematical functions. It allows calling and execution of Matlab (.m) files. However the program slowed down drastically when extensive Matlab code is executed from within Labview. Alternative approach of using mathematical functions in built in Labview is recommended for simple data analysis. It is a recommended that a separate virtual instrument components are written for individual steps so that the speed of the overall process is enhanced.

2.5 Advantages of the Field Emission Experimental System Designed

The advantage of the system that is designed for field emission experiments is the ease with which one could alter any of the following parameters.
1. Voltage applied across the electrodes to assist field emission can be changed dynamically with the help of a user-friendly interface. Both forward and reverse voltage could be applied to any test fixture. This helped in testing the viability of a field emission based CNT diode.

2. Current as low as pico-amps can be measured and plotted as the experiment progresses. Various in built median and averaging filters greatly reduce the noise level of the acquired signal.

3. Temperature of the CNT sample can be precisely controlled and varied from a remote interface. The experiments performed helped in ascertaining that CNTs can be used for high temperature applications. The temperature of the stage can be controlled within an error margin of +/- 5 °C.

4. Pressure of the background gas can be set to a constant value using a bleeder valve and a turbo pump. This helped in conducting experiments to observe the effect of background gas pressure on the field emission characteristics of MWNTs.

5. Type of gas inside the chamber can be selected based on the need. The system has inlets for He, Ar and N₂.

6. Spacing between the cathode and the anode can be set to the desired value using ceramic, quartz or polymer spacers available for different thicknesses. The space between the electrodes could be adjusted for every experiment based on the height of the CNTs grown.

7. Type of electrodes used for the field emission experiments can be changed very easily using the current system. This made experiments with different types of electrodes possible.
3. MWNT SYNTHESIS & CHARACTERIZATION

3.1 Microfabrication

3.1.1 Lithography

CNTs selectively grow on SiO$_2$ surface in a thermal CVD furnace. This is due to the fact that the air-borne catalyst would react with any other surface like Au or Si forming a compound that does not favor the growth of CNTs. The catalyst is left intact on SiO$_2$ surface hence enabling it to start CNT growth [25].

Hence, SiO$_2$ was patterned to grow CNTs in different physical layouts. The CNTs grew only on the SiO$_2$ as expected. The CNTs thus grown in different physical layouts were tested for field emission to study the dependence of the emitted current density on the layout. The two parameters that were varied is pictorially shown in Fig. 3.1

![A single pattern of carbon nanotubes](image)

Size of the island

Space between islands

A single block of CNT islands showing the two variable parameters island size and inter-island space.
Two approaches viz. the lift-off process and the metal etching process was taken to pattern SiO$_2$. A brief introduction highlighting the method involved in each of the approach is given below.

A) The Lift-off Process

The starting material for this process is an oxidized silicon wafer with an oxide thickness of 100 nm. The sample is baked at 110 °C for 8 to 10 minutes on a hotplate to dehydrate the surface. This will promote good photoresist-to-wafer adhesion. It also ensures that the wafer surface is clean and dry.

SC1827 photoresist is then spin coated onto the oxide surface. This is done using Headway Research PWM101 Light Duty Photoresist Spinner. The wafer is held onto a vacuum chuck during this process. Around 5 ml of SC1827 photoresist is dispensed onto the oxide surface and a slow spin of 500 rpm is given initially and is ramped up to 3000 rpm. It is held at this rpm for 30 seconds. This produces a film with a thickness of around 1.2um.

Fig. 3.2 The Lift-off process for patterning SiO$_2$. 

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SC1827 photoresist is then spin coated onto the oxide surface. This is done using Headway Research PWM101 Light Duty Photoresist Spinner. The wafer is held onto a vacuum chuck during this process. Around 5 ml of SC1827 photoresist is dispensed onto the oxide surface and a slow spin of 500 rpm is given initially and is ramped up to 3000 rpm. It is held at this rpm for 30 seconds. This produces a film with a thickness of around 1.2um.
This is followed by soft bake on the hot plate at 95°C for 3 minutes. This step also enhances photoresist-to-wafer adhesion and promotes resist uniformity on the wafer. This step helps in optimizing the light absorbance characteristics of the photoresist. The most important significance of this step is in driving off most of the solvent from the photoresist.

The resist-coated sample is exposed using Oriel UV exposure station. The light source is an 1000 W Hg (Xe) lamp with a wavelength range of ~ 220 to 450nm. It has a digital timer for exposure control with a resolution of 0.1 seconds. The time of exposure = dose required / UV intensity. Dose required to develop SC1827 is 120mJ/cm². If the UV intensity measured is around 12.69 mW/cm² the required time for exposure would be ~ 9.46 seconds.

After the UV exposure is completed the sample is developed using SC354 for 60 seconds. The soluble areas of the photoresist are dissolved by the developer chemical. Visible patterns appear on the wafer. The sample is cleaned with DI water for 5 minutes and dried with N₂ gas. The wafer is then inspected for particles and defects.

The next step is the post-development thermal hard bake on the hot plate at 110 °C for 10 minutes. This will help in evaporating the remaining solvent and also improves resist-to-wafer adhesion. The hard bake is done at a temperature higher than the soft bake.

This is followed by the metal (Cr/Au) deposition using the e-beam evaporation process. E-beam evaporation is done using Temescal BJD-1800 E-Beam Deposition System. The deposition is carried out at an output power of 10KW and a vacuum of 10⁻⁷ Torr. The deposition rate for Au is 3Å/s and for Cr is 2Å/s.

Finally, photoresist lift-off is carried out using acetone in an ultrasonic bath for 1 minute. It is important to remember that generally the lift-off process is used for patterning materials lacking a highly selective etchant and the deposited film thickness should be smaller than the
thickness of the resist. This process was tried inorder to save a metal etching step. This technique is however limited to larger feature sizes.

![Mask used for the liftoff process](image)

<table>
<thead>
<tr>
<th>Size (μm)</th>
<th>Space (μm)</th>
<th>Density Of CNT coverage (%)</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>800</td>
<td>17.122473</td>
</tr>
<tr>
<td>2</td>
<td>400</td>
<td>4.9382716</td>
</tr>
<tr>
<td>3</td>
<td>200</td>
<td>1.3313609</td>
</tr>
<tr>
<td>4</td>
<td>800</td>
<td>22.145329</td>
</tr>
<tr>
<td>5</td>
<td>400</td>
<td>6.25</td>
</tr>
<tr>
<td>6</td>
<td>200</td>
<td>1.6649324</td>
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<tr>
<td>7</td>
<td>800</td>
<td>66.942149</td>
</tr>
<tr>
<td>8</td>
<td>400</td>
<td>18.367347</td>
</tr>
<tr>
<td>9</td>
<td>200</td>
<td>4.8185604</td>
</tr>
</tbody>
</table>

**Fig. 3.3 An example of mask used for the liftoff process**

The mask is made such that the area contained within the red square patterns is covered with chrome. Eventually following the lift-off process as explained earlier the photoresist under this area inside the red square patterns is lifted-off along with the metal on top opening up the SiO₂ underneath.

It can be observed that the patterns in a row numbered 1, 2 & 3 have a constant spacing between CNT islands and the patterns in a column numbered 1, 4 & 7 have a constant size of the CNT islands. This was done to isolate the effects of varying size and spacing on field emission characteristics.
Oftentimes, narrow metal features also lift-off from the substrate at elevated temperatures. The edges obtained using lift-off process was very rough and it was difficult to get well defined square features. This forced the use of an alternative approach to pattern metal over SiO$_2$ which was the metal etching process discussed below.

B) The Metal Etching process

![Diagram of the Metal Etching process for patterning SiO2]

As in the case of the lift-off process the starting material is oxidized silicon wafer with an oxide thickness of about 100 nm. The oxidized silicon wafer is initially baked at 110°C on a hotplate for 8 to 10 minutes as in the case of the lift-off process in order to dehydrate and clean the surface.

10 nm of Cr is deposited on the oxide layer followed by 50 nm of Au using an e-beam evaporation system as mentioned earlier in section 3.1.1. Cr is used as an intermediary layer to promote adhesion between the noble metal Au and SiO$_2$. It is important to note that a very clean
surface should be prepared before metal deposition to avoid pin holes which may result in unwanted growth of CNT in that area causing erroneous results.

SC1827 is spin coated at 3000 rpm for 30 seconds. This resulted in a uniform layer of resist with a thickness of around $1.2\mu m$. Care is taken to ensure that the metal deposition is uniform and devoid of any particles or other irregularities.

The spin coated resist is exposed using an UV exposure station. The exposed resist is developed to obtain the desired windows in the resist layer. Inspection is carried to make sure that the edges of the windows in the resist are sharp. If there is some resist left over the development is carried out again under the same conditions.

After the photoresist development is complete the metals Au & Cr are etched in that order using respective chemical etchants. The sample is inspected again to ensure the quality of windows opened in the metal.

The remaining photoresist is stripped using acetone in an ultrasonic bath for 1 minute. The sample is then used in the thermal CVD furnace for selective CNT growth on the SiO$_2$.

3.1.2 Mask Preparation

The mask was designed as per the requirement for the physical layout using AutoCAD 2004. For the same pattern the mask designed for the liftoff process was complementary to that designed for the metal etching process. During the design of the mask it is very important to make sure that there are no open figures which will result is faulty pattern generation.

The AutoCAD file generated was converted to an ASCII format to suit the pattern generator used to print the mask.

The mask is then printed using GCA Mann 3600 pattern generator. The minimum feature size restriction for the pattern generator is $4\mu m$ and the positioning accuracy is $0.1\mu m$. 
The photoresist AZ1514 on the mask is developed after the exposure is complete. This is followed by rinsing with DI water and drying with N\textsubscript{2} gas. After the photoresist has been developed, chrome etching is carried out. This is followed by cleaning again using DI water and drying with N\textsubscript{2} gas. Finally the remaining photoresist is stripped and the mask is cleaned. It is important to note that these processes take very short time (1-5 minutes) hence care must be taken to avoid over-exposure to chemical etchants.

### 3.2 CNT Synthesis – Thermal Chemical Vapor Deposition

Thermal chemical vapor deposition (TCVD) synthesis is achieved by putting a carbon source in the gas phase and using an energy source, such as a resistively heated coil, to transfer energy to a gaseous carbon containing molecule. The gaseous carbon source used was xylene. The energy source is used to "crack" the xylene molecule into reactive atomic carbon. Then, the carbon diffuses towards the substrate which is heated. The catalyst (usually a first row transition metal such as Ni, Fe or Co) which initiates the CNT growth is supplied in the gas phase as ferrocene. The ferrocene molecule breaks as a result of the thermal energy provided and the catalyst is deposited on the substrate. The catalyst does not react with SiO\textsubscript{2} and hence is left intact on the oxide layer whereas it reacts with Au or Si forming a compound that does not support CNT growth. The reactive carbon that diffuses towards the hot substrate binds with the catalyst over the oxide layer. CNTs will be formed if the proper parameters are maintained. Excellent alignment [26], as well as positional control on nanometer scale [27], can be achieved by using CVD. Control over the diameter, as well as the growth rate of the nanotubes can also be maintained. The appropriate metal catalyst can preferentially grow single rather than multi-walled CNTs.
The nanotubes were grown in a CVD tube furnace system from a vapor-phase mixture of xylene \([C_8H_{10}]\) and ferrocene \([\text{Fe(C}_5\text{H}_5)_2]\). A 0.01 g/mL solution of ferrocene in xylene was preheated at about 150 °C and sublimed into the CVD chamber. Prior to this, the chamber was pumped to a 10^{-3} Torr vacuum, backfilled with flowing argon to ~ 100 mTorr and heated gradually to 800 °C.

Under this growth condition, ferrocene is the nanotube nucleation initiator and xylene the carbon source. This precursor combination results in the selective growth of 20-30-nm-diameter multiwalled CNTs on SiO\(_2\) surfaces. No nanotube growth is observed on Au surfaces or on the native SiO\(_2\) layer. The growth rate is ~ 10\(\mu\)m/minute.
3.3 Electron Microscopy of CNTs Grown

A) Scanning electron microscopy (SEM): SEM measurements were carried out in a Hitachi S-4500II Field Emission SEM equipped with a field emission gun operated at 20 keV. Fig. 3.6(a) shows CNT grown on square islands of SiO$_2$ patterned by opening windows in Cr/Au. The sharp edges achieved can be seen from the Fig. 3.6(b). The Fig. 3.6(c) shows vertically aligned Carbon Nanotubes with a length of around 60um.

Fig. 3.6 (a) Islands of CNT grown over patterned SiO$_2$. (b) A single island of carbon nanotube. (c) Cross-sectional view of the CNT grown.
B) Transmission electron microscopy (TEM): The structures of individual nanotubes were probed by conventional and high-resolution transmission electron microscopy (TEM) measurements. Figure 3.7 shows the microstructure of a MWNT with around 25 walls. The tube is hollow and the outer walls appear ruptured.

(a) Strands of Multiwalled CNTs observed under the TEM.

(b) An image of a single multiwalled CNT magnified 10 times when compared to the Fig 3.7 (a).

Fig. 3.7 TEM image showing the microstructure of the MWNT
4. FACTORS EFFECTING FIELD EMISSION FROM MULTIWALLED CARBON NANOTUBES: RESULTS & OBSERVATIONS

Field emission from CNTs is dependent on multiple factors as discussed in chapter 1. As part of this thesis, tests have been carried out to observe the dependence of field emission from CNT on factors like its temperature, the type of gas environment, the background pressure during field emission, alignment of CNTs, the substrate used for CNT growth & the conditions during growth. The test fixture constructed for the experiments can be seen in Fig. 4.1.

![Test Fixture Diagram]

Fig. 4.1 A simplified sketch showing the test fixture used for the experiments.
The sandwiched electrode structure can be seen from the Fig. 4.1. The electrodes are spaced apart using polymer, quartz or ceramic spacers. A 14 um thick aluminum foil is used to connect the patterned gold surface to the copper cathode at the bottom. This is done to avoid a voltage drop in the insulating SiO$_2$ layer. The sandwiched electrode structure is placed on a stage whose temperature can be precisely controlled over a range of 30 °C to 800 °C. Gold coated quartz slab was used initially as the electrode because it offered very high flatness. However it suffered from excessive damage due to repeated field emission experiments. This forced the need for using copper electrodes which had to be polished extensively after each experiment to clean and obtain a smooth surface. The entire fixture shown in Fig. 4.1. is mounted inside a vacuum chamber to precisely control the ambient pressure of operation. The experimental results obtained using this test setup are discussed below.

4.1 Effect of CNT Temperature Variation

The experiment involved setting the CNT sample on a temperature controlled stage mounted inside the vacuum chamber. During the experiment the electric field applied between the anode and cathode was set at 3 V/um. In step-1, the temperature was ramped-up to 200 °C in a span of 1 hour while the field emitted current was continuously monitored. In step-2 as field emitted current was being measured the CNT sample was allowed to cool back to the room temperature which took around 4 hours. Step-3 involved repetition of step-1, however it can be observed that during this step, the field emitted current very closely followed the profile in step-2. “Self-cleaning” is reported by Gupta et al. as a process where the adsorbates are partially depleted and the nanotube surface is brought to a new steady state while it is being heated [28]. It is observed that in step-1 during the initial part of the heating process the field emitted current deviates from the subsequent profile that it follows in step 2 & 3. This is attributed to the self-
cleaning process of desorption of gas molecules from the CNT surface combined with the out-gassing from the cathode that is heated. During step-1, the background pressure was noticed to increase from $1 \times 10^{-7}$ to $8 \times 10^{-7}$ Torr. The adsorbed species has not yet been identified. The experimental result observed is shown in the Fig. 4.2. It is important to note that the CNT growth using the Thermal CVD process used does not produce metallic or semiconducting CNTs selectively. The experiment was performed at 3V/um to demonstrate that a temperature rise would cause an increase in field emitted current thus lowering the turn-on voltage for field emission.

![Current Density Vs Temperature (3V/um)](image)

**Fig. 4.2 Dependence of Field Emitted Current from Multi-Walled Carbon Nanotubes on its temperature.**
The various possible effects of increasing CNT temperature are discussed below.

1. The observed increase in the field emitted current as a consequence of increasing the temperature of the CNT sample could be a result of an overall decrease in the effective work function of the CNT emitter. The change in work function could be due to one of the following possible reasons.

   a) Thermal expansion causing structural changes could result in a change in CNT work function [29].

   b) Desorption of gas molecules from the surface could alter the work function of the CNT [30,31].

   c) A possible chemical reaction at the surface of the CNT could have an effect on its work function [32].

   d) A variation in the Fermi energy level due to thermally induced carrier generation would cause a change in the CNT work function. If the CNT is assumed to be doped the Fermi energy level would move towards the Intrinsic energy level with rise in temperature [33].

Fig. 4.3 Change in Fermi level with rise in temperature of a doped semiconductor [1].
e) There is a possibility of the CNT getting doped with the catalyst/impurities as a result of diffusion from the substrate while it is being heated. This could also alter the CNT work function.

2. The component of Thermionic emission in the measured current becomes prominent at high temperatures and low electric fields. ‘Richardson- Dushman’ equation, dating from 1923, describes the current density emitted by a heated filament, as \[ J(T) = A T^2 \exp(-\phi/kT) \], the value of \( \phi \) is referred to as the ‘Richardson’ work function. It is important to note that there is an intrinsic T-dependence of the workfunction [34]. However as the temperature in the experiments performed was not very high this effect might not be of a great significance.

3. A difference in thermal expansion co-efficients of the substrate and CNT could induce stress at the CNT-substrate interface. This could result in possible uprooting of the CNT at high applied electric fields causing a decrease in the overall emitting area. This being so, an overall increase in the current with rise in temperature is observed which forces one to believe that decrease in emitter work-function could be the most dominating factor at higher temperatures.

4. It is believed that the temperature and high current induced self-heating decreases the contact resistance at the CNT-substrate interface which will be very significant when the field emission device is operated at low voltages and high currents.

The result obtained as shown in Fig. 4.2 is in agreement with the data reported by Gupta et al [28]. It can be seen from Fig. 4.4 that the applied electric field being kept constant as the temperature of the CNT is allowed to increase from room temperature to 500°C, the intensity of the spot on the phosphor screen placed above the field emitter initially increases reflecting a rise in the field emitted current however as the temperature is increased further a saturation of the emitted current is observed.
Fig. 4.4 The intensity of the spots on a phosphor screen due to field emission is observed to increase with temperature. From reference [28] with permission (Appendix: C9).

Current saturation is also observed at high temperatures during the experiments performed. This is evident from the Fig. 4.5.

Fig. 4.5 Variation of current Density with temperature showing saturation at high temperature.

It is believed that as the temperature of the CNT sample is increased gradually the emitted current becomes large enough causing the space charge effect due to ionized gases as
well as emitted electrons to become prominent. The increase in space charge in the vicinity of
the emitter results in a decrease in the Electric field near the tip which in turn causes an increase
in the width of the energy barrier which the field emitted electrons have to tunnel through, thus
causing a saturation of the emitted current [36, 37]. The current saturation observed at high
temperatures could also be a result of a decrease in the effective emitting area of CNTs as a
consequence of temperature induced damage.

4.2 Effect of Background Pressure Variation

Experiments were performed to observe the effect of increasing the background pressure
in steps of 1 order of magnitude. The multiwalled CNT sample (grown using the thermal CVD
setup discussed in section 3), was initially mounted inside the vacuum chamber and the pressure
is lowered to $1 \times 10^{-6}$ Torrs. This is followed by flushing the chamber with N$_2$ back to atmospheric
pressure. This cycle of evacuating and flushing is repeated several times to ensure that there is no
other gas besides N$_2$ present inside the chamber. This is followed by sweeping the applied
voltage and measuring the field emitted current at different background pressures ranging from
$1 \times 10^{-6}$ Torr to $1 \times 10^{-4}$ Torr. The results obtained are shown in Fig. 4.6, Fig. 4.7 and Fig. 4.8.

The various possible effects of increasing the background gas pressure are as follows.

a) Adsorption of gas molecules on the CNT surface increases with the background pressure
   until a saturation is reached. This would result in a change in work function of the
   emitter.

b) As the background pressure in the chamber is increased the component of gas ionization
   current begins to dominate.

c) If the temperature, applied electric field, and the inter-electrode distance are kept constant
   and the background pressure increased gradually, at a certain value of pressure, unique to

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the gas being used, negatively charged plasma (CNT emitter sample is mounted on the cathode) begins to appear causing arcs between the anode and the cathode.

d) Bombardment by positively charged ions present in the vicinity of the emitter could result in CNT surface degradation.

e) Damage caused to the gold plated surface surrounding the CNT patterned islands resulting in sharp edged craters might cause an increase in the background noise in the current measured.

f) The columbic field generated by the positively charged gas ions in the vicinity of the emitter is dominant at high background pressures. This space charge effect at high background pressures could result in an increase in the width of the potential barrier resulting in a decrease in the field emission current

Fig. 4.6 (a)

Fig. 4.6 Effect of change in background pressure of Nitrogen on field emitted current. (fig. contd.)
As the pressure is increased, the field emitted current decreased and the turn-on voltage is also observed to increase. This is not desirable, hence it is essential to have lower background pressure in order to increase the field emitted current. It is true that few adsorbates present on the CNT surface improve field emission when compared to a very clean CNT surface [38, 39]. However, at pressures of the order $10^{-5}$ Torrs and greater, any increase in the background pressure proves detrimental to the field emitted current. This is true irrespective of the different types of gases used for experimentation.
Fig. 4.7 Effect of change in background pressure of Helium on field emitted current.
Fig. 4.8 Effect of change in background pressure of Argon on field emitted current.
Similar trend of decrease in field emitted current and increase in the turn-on voltage with rise in background pressure is observed in the case of Helium and Argon also.

For common field emitters made of metals (e.g., tungsten), the emitter surfaces are damaged easily and significantly by bombardments of gas ions. For MWNTs, on the other hand no serious damage is observed owing to its robustness [39].

### 4.3 Dependence on the Background Gas Species

The CNT sample is mounted inside the vacuum chamber before pumping down the chamber to lower than $1 \times 10^{-6}$ Torr. This is followed by heating the sample in vacuum to around 500 °C to facilitate surface cleaning. The CNT is then allowed to cool back to room temperature. After this stage Helium is passed into the chamber such that the pressure is close to $10^{-6}$ Torrs. The field emission experiment is then performed by increasing the voltage in steps recording the emitted current. The same procedure is carried out for Argon and Nitrogen as well. The experiment with all the gases was performed at a pressure of $10^{-6}$ Torr. The results obtained are shown in Fig. 4.9.

![Effect of Different Gas Species on Field Emission](image)

Fig. 4.9(a)

Fig. 4.9 Effect of change in background gas species on field emitted current. (fig. contd.)
Different gases interact with the CNT surface in a different way which is the reason for the observed variation in the field emitted current as the background gas species is changed. The field emitted current depends strongly on the work function and geometry of the surface, and thus is very susceptible to gas exposures [12].

Adsorption of molecules causes a charge transfer and is believed to determine the direction of the dipole field at the CNT edges. It is assumed that the adsorbed gas species causes a shift in the Fermi level (a change in the work function) which in turn changes the available density of states near the Fermi level [38]. This would directly influence the field emitted current. However the different interaction mechanism for individual gas species is not clear.

It is believed that Nitrogen and Argon tends to degrade the emitter whereas He is observed to cause relatively no degradation [40]. This can be inferred from the results in Fig. 4.9.  

4.4 Dependence on CNT Orientation (Random Vs Aligned)
It can be seen from Equation 1.2 that the field enhancement factor plays a key role in boosting the field emission current from a CNT. In the case of a randomly grown CNT sample as shown in Fig. 4.10 (a) the field enhancement factor is poor and the electrical screening effect becomes predominant. The electrical screening effect results in a decrease in the effective emitter area because the tips of the short nanotubes do not see a high electric field owing to the presence of neighboring taller nanotubes. The field emission results obtained can be seen from Fig. 4.11.

Fig. 4.10 (a) Random and (b) Aligned CNT tested for field emission.
It can be seen from the data obtained that an alignment in the CNT grown greatly enhances the field emission characteristic. It has also been observed that even though the random CNTs have poor field emission characteristics they tend to offer better life time [8]. This could
be due to the way they are oriented giving better mechanical strength to bear the electrostatic force acting on them during field emission.

4.5 Effect of the Substrate Material Used for Growth

The substrate material has a substantial influence on the field emitted current density as well as on the turn-on electric field as observed in fig 4.12. It is evident that metallic substrates are superior to non-metallic ones.

There are various ways in which an underlying substrate can influence field emission.

1. The type and structure of CNT grown depends on the substrate used [20]. This has been observed during characterization done on the CNTs.

2. The strength with which the CNT holds on to the base material depends on the type of substrate. During CNT growth, an amorphous substrate like SiO$_2$ could give a better physical adhesion to the CNT grown than a crystalline metallic substrate like Nickel. This could control the lifetime of a CNT emitter.

3. The electrical conduction mechanism within the substrate material under different conditions of operation (viz. temperature, voltage) varies depending on its type.

4. The breakdown mechanism at high temperature or applied electric field depends on the type of substrate used. Metallic substrates tend to suffer from thermal runaway at high current densities and elevated temperatures of operation.

5. The background field emission which accounts for the noise in the measured current depends on the morphology of the substrate employed. A highly smooth substrate surface is ideal for use.

6. The contact resistance depends on the nature of the CNT-substrate interface.
Fig. 4. Effect of the type of substrate on field emitted current.
4.6 Other Experimental Observations

4.6.1 CNT Emitter Degradation

It is observed that the CNT field emitter suffers a gradual degradation as a result of multiple rounds of field emission experiments. The islands of patterned CNT emitters tend to leave an imprint on the anode surface. As a result of emitter degradation some of the imprints disappear after subsequent rounds of field emission experiments. This can be observed in Fig. 4.13. The image has a magnification of 5.

Fig. 4.13 Few of the imprints on the anode surface disappear after each experiment owing to CNT degradation.
The degradation mechanism is not very clear. Few possible reasons for degradation are suggested here.

a) As a result of poor adhesion to the substrate CNTs have a tendency to get uprooted at high applied electric fields due to electrostatic force acting on them [11].

b) The residual oxygen in the chamber may cause oxidative etching.

c) Bombardment by charged gas ions may cause damage to the CNT emitter surface.

d) Arcing between the electrodes could cause significant damage to the CNTs.

e) High contact resistance at the base of the CNT might result in excessive joule heating at high current densities resulting in significant damage.

It can be observed from Fig. 4.14 that the damage is caused as a result of the CNT getting uprooted and not because of an arc. Damage due to an arc tends to destroy even the substrate in that region which is not found in this case.

Fig. 4.14 SEM picture showing emitter degradation as a consequence of field emission. The picture shows the region on the substrate where the CNTs have been uprooted.
Degradation at low applied fields is believed to be due to mechanical failure at the contact whereas at high electric fields resistive heating and mechanical stress at the CNT-substrate interface could do the damage [11].

4.6.2 Anode Degradation and Heating as a Result of Field Emission

Localization of emission and large currents from CNTs result in significant anode heating.

Fig. 4.15 (a) Imprint observed on the copper anode after field emission (b) Visualization of ring pattern on anode observed by Walker et al.[45].

Cross-sectional current from MWNT reveals a ring like current density indicative of emission from the nanotube ends. This behavior could produce extremely large local current densities within the ring which could significantly damage the anode.

If the anode temperature increases drastically electrons that reach the anode surface after traversing through the vacuum gap could get back-scattered instead of being received by the anode. This phenomenon could distort the field between the electrodes.
In actual field emission applications, the vacuum gap is of the order of tens of microns and current densities are large as a result of decreased radial spreading. Hence the effect of anode heating is expected to be more pronounced [46]. Due to the degradation that occurred, the copper anode was re-polished after every experiment.

The damage to the gold plating shown in Fig 4.16 is a result of multiple rounds of experiments. The gold is observed to get pealed which may be due to a combined effect of electron bombardment as well as joule heating.

Fig. 4.16 Damaged surface of a gold plated quartz anode.

The temperature rise of the anode due to emission from a single CNT is not significant enough to damage the device however the temperature increase due to many CNTs could cause damage to the anode as shown by Fisher and Walker [45]. The radial temperature profile was estimated by the following expression

\[
T(R) = \frac{IV}{2\pi \kappa R}
\]  

(4.1)

Where \(IV\) is the total power from the electron beam, \(\kappa\) is the thermal conductivity of anode material and \(R\) is the distance from the center of the beam [45].

Bombardment of the anode with energetic electrons especially at high applied electric fields results in large heating rates at the anode. Practical devices have isolated small anode areas
which could create problem of continuous heat dissipation during its operation. For devices designed to carry large current densities, anode heating can cause erosion or catastrophic failure of the device.

### 4.6.3 Young’s Interference Fringes

Electron beams can be treated as waves which interfere either constructively or destructively depending on the phase shift caused by the different path lengths of the electrons. If the geometrical configuration of the two emission sites causes a phase shift of $\pi$ it results in destructive interference resulting in a dark line in the interference fringes. If the phase shift is $2\pi$ it results in constructive interference corresponding to a bright line.

Young’s interference fringes have been found after field emission experiments on the copper anode surface as an imprint.

As reported by T. Yamashita et al., the Fig. 4.17 shows how chemisorption of molecules on emission sites results in bright spots with young’s interference fringes in the background.

![Fig. 4.17 Typical Field emission microscope (FEM) image of a MWNT during field emission. From reference [47] with permission (Appendix: C10).](image)
Bright spots as well as the interference fringes were observed after the field emission experiment. It is known that the electron beam spreads as a result of coulomb interaction however the initial ring is preserved [46]. The concentric nature of the interference fringes (fig 4.18) verifies the flatness of the anode with respect to the emitter.

Fig. 4. 18 Young’s interference fringes found on the anode surface

Temperature was observed to have a significant effect in increasing the field emitted current from multiwalled CNTs. Deterioration in field emission characteristics with increase in the ambient pressure of operation was noticed. Dependence of field emission from multiwalled CNTs on the type of surrounding gas was established. The relation between the alignment of the MWNTs grown and their field emission characteristics was studied. Different types of substrates were used for CNT growth and the various ways it affects the field emission properties were analyzed. Other experimental observations like CNT emitter damage, anode heating and formation of young’s interference fringes have been reported.
5. CONCLUSION AND SUGGESTIONS FOR FUTURE RESEARCH

5.1 Summary and Conclusions

Discussion of the basic physics that governs field emission including the different aspects of the Fowler Nordheim Model has been given in chapter 1. Different factors that affect field emission from MWNTs have been discussed. Different parameters that can be controlled in order to optimize field emission are highlighted and analytical expressions showing how these variables influence the net field emitted current are mentioned. Some of the existing works on similar topics in the literature are visited and their important results are magnified. Detailed analysis of the experimental requirements was carried out. System to study the effect of various factors on field emission from MWNTs was designed and assembled. The main features and advantages of the system have been discussed in chapter 2. Results of the field emission experiments performed and various observations made have been discussed in chapter 4. Experimental results have been explained with analytical discussions wherever possible. The main goal of the experiments performed was to identify the relation between field emission from MWNTs and the various factors that influenced it. The results obtained will be useful in choosing the conditions for operation of a field emission device.

One of the contributions of this work is that it shows how temperature affects the field emitted current density. Contrary to the belief that field emission is relatively insensitive to temperature changes, it has been shown that variations in temperature have a significant effect on the field emitted current from MWNTs. One of the reasons for this may be the change in the CNT emitter work function as a result of heating. This result shall be critical for high temperature applications of CNT field emission based devices.
At relatively poor vacuum in the range of $10^{-6}$ Torrs to $10^{-3}$ Torrs it has been observed that any increase in pressure results in deterioration of the performance of CNT field emitters. This effect of pressure on field emission has been verified with three different types of gases viz. Ar, He and N$_2$. This result could be made use of in pressure sensing applications.

It has been demonstrated that a change in the background gas species affects the field emission from CNTs all other parameters remaining the same. Effect of CNT alignment and the substrate used for CNT growth on the field emission characteristics have been reported. It has been shown that conditions during growth also have an impact on the FE property.

Other important experimental observations have been made. CNT emitter degradation and the various possible mechanisms that could cause it have been discussed. Anode surface degradation and heating as a result of field emission has been reported. Young’s interference rings have been observed on the anode surface as a consequence of field emission.

The results obtained as part of this work can be used to optimize the performance of a MWNT based field emission device in terms of the field emitted current density and the required turn-on voltage.

5.2 Prospects & Limitations

Today the most mature technology to produce gated micro field electron emitter arrays is the so called Spindt-type metal micro-tip process. The drawbacks of the Spindt-type process are expensive production technique, relatively poor lifetime in technical vacuum and the high operating voltages required. CNTs can be regarded as the potential second-generation technology to Spindt-type metal micro-tips. The use of CNTs as field enhancing structures in electron emission sources can bring several advantages such as longer lifetime and operation in poor vacuum due to the high chemical inertness as well as low operation voltages and perhaps most
important of all is its very low cost production technique. CNTs do not suffer from thermal runaway at high temperatures (except metallic CNT). However emitter degradation at high emission currents limits the full exploitation of high emission site density that can be achieved using CNTs. The emission degradation becomes apparent for emission currents in the microamps range for a single emitter. High power dissipation could be a cause for the damage. Therefore, although the fundamental properties of CNTs are very favorable for the use as field emission tips, these properties alone will not guarantee their success in this area. A perfect control of the catalytic CNT growth process is needed for the success of CNT field emitter technology, more so for high current applications.

5.3 Suggested Enhancements in the Experimental System

The suggested improvements to the experimental system designed are discussed below
a) A modification in the Labview program incorporating a faster data acquisition algorithm would help in reducing the time taken for each experiment which is currently around 4 hours.
b) The contacts between the power feed-through, wires and the electrodes should be modified to reduce the noise level. This would become crucial while making very low current measurements (< 10 nA).
c) The size of the vacuum chamber used should be reduced to achieve higher vacuum level. A pressure controller is required to accurately control the pressure inside the chamber. The current method used is prone to minor fluctuations.
d) A voltage source that could supply voltage higher than 5 KV would be very beneficial.
e) Inter-electrode spacing is currently adjusted using ceramic, quartz or polymer spacers. Once the spacing is fixed it is not possible to adjust it without breaking the vacuum in the chamber. It would be advantageous to have a dynamically adjustable system using a linear motion feed
through as shown in Fig. 5.1 that would avoid opening the chamber every time the inter-electrode distance has to be altered.

![Image of feed-through](http://209.238.89.157/series.asp?series=L-2141)

Fig. 5.1 A linear motion feed-through from Huntington Mechanical Laboratories, Inc. that could be used for precise control of inter-electrode spacing. Retrieved from http://209.238.89.157/series.asp?series=L-2141 with permission (Appendix: C11).

f) A feed through for an optical probe could be installed in order to study photoemission that is occurring during electric field assisted electron emission.

### 5.4 Suggestions for Future Research

More research is required to be done in the area of CNT synthesis in order to be able to repeatedly grow well aligned, long and identical CNT samples.

Experiments need to be carried out to study field emission from MWNT at temperatures lower than the normal room temperature. This can be achieved with the help of the cooling stage S2 using liquid nitrogen.

It would be interesting to inject precise amounts of different gases under conditions of ultra high vacuum and study its effect on CNT field emission. Research needs be done in order to materialize device applications to this thesis work carried out.

Further study of the effects of varying physical layout of CNTs on its field emission performance should be conducted. Studies could be carried out in order to check for any photoemission occurring during the process of field emission. Research should be done to investigate the effects of doping & surface treatment on FE characteristics.
It is also important to study how field emission depends on various device configurations including a planar design. Simulations should be carried out to understand the influence of various experimental and growth related factors on field emission from MWNTs. Tools written using Matlab 7.0 for data analysis & curve fitting (Appendix B) can be used for this purpose.
REFERENCES


[31] Noejung Park, Seungwu Han and Jisoon Ihm, “Effects of oxygen adsorption on carbon nanotube field emitters”, Physical review B, volume 64, 125401


[37] Igor S. Altman, Peter V. Pikhitsa, and Mansoo Choi, “Two-process Model of Electron Field Emission from Nanocarbons: Temperature effect”


APPENDIX A: EXPERIMENTAL SYSTEM AUTOMATION USING LABVIEW

A1. Initialize Voltage Supply

![Diagram of Voltage Supply Initialization process using LabVIEW]
A2. Set Voltage Value

![Diagram of voltage setting process with voltage readings and iteration current values.]
A3. Initialize Picoammeter

- `*RST;`
- `*IDNP;`  
- `256`
- `Func:CURR`
- `%2f`

**6485 GPIB Add**

**Instrument 6485 ID 2**

**NPLC 2**

**Auto Zero 2**

**Error Out**

**Error In**

**Syst:ZOH ON**

**Syst:RANG:AUTO ON**

**INIT**

**Syst:ZCOR:ACQ**

**Syst:ZCOR ON**

**Syst:ZOH OFF**
A4. Measure current
A5. Create output data file and generate plots

Voltage measured
1500

49830

Current measured (nA)
217000

Please enter a file name:

create or replace

Chart length (points) 2

I-V Curve 2

Fowler-Nordheim plot 2

Instance

I-V Curve 3

Instance
I-V Curve

Fowler-Nordheim plot
APPENDIX B: TOOLS FOR DATA ANALYSIS DEVELOPED USING MATLAB

B.1 Program to generate multiple plots

```matlab
a=[];
b=[];
f=[];
[a]=xlsread('C:\abhilash\data\test.xls');
siz1 = size(a);
siz1 = siz1(1,1);
for i=1:siz1
    if a(i,2)>0
        a(i,4)=log(a(i,2)/((a(i,1)).^2));
        a(i,3)=1/a(i,1);
    end
end
j=1;
for i=1:siz1
    if (a(i,1)>1200)
        f(j,1)=a(i,3);
        f(j,2)=a(i,4);
        j=j+1;
    end
end
fsiz=size(f);
```
fsiz = fsiz(1,1);
FNfit = polyfit(f(1:fsiz,1),f(1:fsiz,2),1);
p = exp(FNfit(1,2));
q = -1*FNfit(1,1);
for i = 1:a(size1,1)
    b(i,1) = i;
    b(i,2) = p*i*i*exp((-1*q)/i);
    b(i,3) = 1/i;
    b(i,4) = polyval(FNfit,1/i);
end
siz2 = size(b);
size2 = siz2(1,1);

scrsz = get(0,'ScreenSize');
figure('Position',[10 65 (3*scrsz(3))/4+20 (3*scrsz(4))/4+80]);

subplot(3,1,1); plot(a(1:size1,1),a(1:size1,2));...
xlabel('Voltage Applied(V)','FontSize',10);ylabel('Current Measured(A)','FontSize',10);grid on;
subplot(3,1,2); plot(a(1:size1,3),a(1:size1,4),'.',b(50:size2,3),b(50:size2,4));...
xlabel('1/V','FontSize',10);ylabel('Ln(I / V^2)','FontSize',10); grid on;
subplot(3,1,3); plot(a(1:size1,1),a(1:size1,2),b(1:size2,1),b(1:size2,2),'.');...
B.2 Program for data analysis and curve fitting

% Current is in Amperes
% Area is in m2
% Work function is in electron volts
% Voltage is in Volts
% Inter-electrode distance is in m
% Field enhancement factor is a dimensionless quantity

clear;
format long e;
prompt = {'Please enter the complete path for the data (.xls) file' , ...
              'Please enter the Inter-electrode distance (in m)' , ...
              'Please enter the effective area of emission(in m2)' , ...
              'Please enter notes if any'};
dlg_title = 'Inputs required for data analysis';
num_lines= 2;
def = {'c:\Documents and Settings\Eashwar\My Documents\abhilash\data.xls',...
'0.000150', ...
'0.0001', ");
answer1 = inputdlg(prompt, dlg_title, num_lines, def);

r=[];
d=[];
a=[];
fn=[];
point=[];
j=1;

[r] = xlsread(char(answer1(1)));
r(any(isnan(r)'), :) = [];
d=str2double(char(answer1(2)));
a=str2double(char(answer1(3)));
siz1 = size(r);
size1 = siz1(1,1);

for i=1:size1
r(i,3)=r(i,1)/d;
    if r(i,2)>0
    fn(j,1)=1/r(i,3);
    fn(j,2)=log(r(i,2)/((r(i,3)).^2));
    j=j+1;
end
j=j+1;
end
end

siz2 = size(fn);
size2 = siz2(1,1);

subplot(2,1,1); plot(r(1:size1,1),r(1:size1,2),'-or');...
xlabel('Voltage','FontSize',10);ylabel('Current','FontSize',10); grid on;
subplot(2,1,2); plot(fn(1:size2,1),fn(1:size2,2),'-og');...
xlabel('1/E','FontSize',10);ylabel('Ln(I / E^2)','FontSize',10); grid on;

prompt = {'Please enter the point where you want the fit to begin'};
dlg_title = 'Inputs required for data analysis';
num_lines= 2;
def   = {'0.0000001577'};
answer2  = inputdlg(prompt,dlg_title,num_lines,def);
point=str2double(char(answer2(1)));

j=1;
fnfit=[];
for i=1:size2
    if (fn(i,1)<point)
        fnfit(j,1)=fn(i,1);
        fnfit(j,2)=fn(i,2);
    end
end
j=j+1;
end
end

siz3=size(fnfit);
size3=siz3(1,1);
fnpolyfit=polyfit(fnfit(1:size3,1),fnfit(1:size3,2),1)

minval=min(fn(1:size2,1));
maxval=max(fn(1:size2,1));
j=maxval;
step=((maxval-minval)/1000);

fnpolyval=[];
for i=1:size3
    fnpolyval(i,1)=fnfit(i,1);
    fnpolyval(i,2)=polyval(fnpolyfit,fnfit(i,1));
end

siz4=size(fnpolyval);
size4=siz4(1,1);
m=[];
c=[];
m=fnpolyfit(1,1);
c=fnpolyfit(1,2);
phi=[];
phi=0;
difference=1;

conv=[];
j=1;
change=1;
valnew=0;

while (change>0.0001)
phi=phi+0.01;
valold=valnew;
valnew=log(a*(0.0000015/phi)*((6440000000*((phi.^1.5)/m)).^2))+(10.4/(phi.^0.5));
difference=c-valnew;
change=abs(valold-valnew)
conv(j,1)=phi;
conv(j,2)=valnew;
j=j+1;
end

valnew

phi

gamma=-(6440000000*((phi.^1.5)/m))
siz5=size(conv);
size5=siz5(1,1);

subplot(1,1,1);plot(conv(1:size5,1),conv(1:size5,2),'-*r');...
xlabel('phi','FontSize',10);ylabel('val','FontSize',10); grid on;
clear;
APPENDIX C: PERMISSION TO USE COPYRIGHTED MATERIAL

C1.

From: "Jean-Marc Bonard" <jmbonard@gmx.ch>
To: "Abhilash Krishna" <akrish2@lsu.edu>
Subject: Re: Permission to use figure
Date: Mon, 20 Jun 2005 21:03:43 +0200

Dear Mr. Krishna,

---------------------------------------------------------------
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I would really appreciate if you could grant me the permission to use your figure.

-------------------------------------------------------------------
There's absolutely no problem - please feel free to use the figure.
And many thanks for your interest in our work!

Good luck for your thesis,

Kind regards,

Jean-Marc Bonard

C2.

From: RIGHTS <Rights@aip.org>
To: akrish2@lsu.edu
Subject: Re: Permission to use figure
Date: Fri, 24 Jun 2005 12:09:26 -0400

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Figs. 2 and 3

Fig. 4

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Otto Zhou

Lyle Jones Distinguished Professor
Curriculum in Applied and Materials Sciences
Department of Physics and Astronomy
CB 3255 Phillips Hall
Chapel Hill, NC 27599
Tel: 919-962-3297
FAX: 919-962-0480
e-mail: zhou@physics.unc.edu
website: www.unc.edu/~zhou

-----Original Message-----
From: Abhilash Krishna [mailto:akrish2@lsu.edu]
Sent: Monday, June 20, 2005 2:12 PM
To: zhou@physics.unc.edu
Subject: Permission to use figure

Dear Dr.Otto Zhou

I am Abhilash Krishna, a master's student at Louisiana State University. My master's thesis is on Factors effecting field emission from MWNTs.

For the purpose of adding in my thesis report, I would like to use the figure 4 in your research paper whose details are given below.


I would really appreciate if you could grant me the permission to use your figure.
Thank you very much for your time.

Best Regards.

Abhilash Krishna

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From: "Yuan Cheng" cheng@physics.unc.edu
To: "AbhilashKrishna"<akrish2@lsu.edu>
Subject: Re: Permission to use figure
Date: Mon, 20 Jun 2005 15:29:49 -0400

Hi Abhilash,

You can use the figure any way you want with full credit to the original publication.

Thank you for your interest in my paper. Please feel free to contact me again if I can be of further assistance.
best,
Yuan Cheng

----- Original Message ----- 
From: Abhilash Krishna
To: cheng@physics.unc.edu 
Sent: Monday, June 20, 2005 2:32 PM 
Subject: Permission to use figure 

Dear Dr. Yuan Cheng

I am Abhilash Krishna, a master's student at Louisiana State University. My master's thesis is on Factors effecting field emission from MWNTs. For the purpose of adding in my thesis report I would like to use the figure 3 in your research paper whose details are given below.


I would really appreciate if you could grant me the permission to use your figure.

Thank you very much for your time.

Best Regards.

Abhilash Krishna
Yes, you can use them.

Zhifeng

At 05:31 PM 6/21/2005, you wrote:

Dear Dr. Zhifeng Ren

I am Abhilash Krishna, a master's student at Louisiana State University. My master's thesis is on Factors effecting field emission from MWNTs. For the purpose of adding in my thesis report, I would like to use the figure 2 & 4 in your research paper whose details are given below.


I would really appreciate if you could grant me permission the to use the figures

Thank you very much for your time.

Best Regards.

Abhilash Krishna

Zhifeng Ren, Professor
Department of Physics
Boston College
Chestnut Hill, MA 02467
Phone: 617-552-2832
Fax: 617-552-8478
http://www.physics.bc.edu/faculty/Ren.html

Of course - please go ahead
Best of luck with your thesis

Bill Milne

At 20:14 20/06/2005, you wrote:

Dear Dr. W. I. Milne

I am Abhilash Krishna, a master's student at Louisiana State University. My master's thesis is on Factors effecting field emission from MWNTs. For the purpose of adding in my thesis report, I would like to use the figure 6 in your research paper whose details are given below.


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Thank you very much for your time.

Best Regards.

Abhilash Krishna

C7.

From: "N S Xu" stsxns@zsu.edu.cn
To: "Abhilash Krishna" <akrish2@lsu.edu>
Subject: Re: Permission to use figure
Date: Wed, 22 Jun 2005 09:24:14 +0800

Yes. Thank you for letting me know.

NSX
----- Original Message ----- 
From: "Abhilash Krishna" <akrish2@lsu.edu>
To: stsxns@zsu.edu.cn
Sent: Tuesday, June 21, 2005 4:19 AM
Subject: Permission to use figure
Dear Dr. N. S. Xu,

I am Abhilash Krishna, a master's student at Louisiana State University. My master's thesis is on Factors effecting field emission from MWNTs. For the purpose of adding in my thesis report, I would like to use the figure 1 in your research paper whose details are given below.

Shi-Dong Liang and N. S. Xua, “Chirality effect of single-wall carbon nanotubes on field emission” Applied physics letters volume 83, number 6, 11 august 2003.

I would really appreciate if you could grant me the permission to use your figure.

Thank you very much for your time.

Best Regards.

Abhilash Krishna

C8.

From: "Young Hee Lee" leeyoung@skku.edu
To: "Abhilash Krishna" <akrish2@lsu.edu>
Subject: Re: Permission to use figure
Date: Tue, 21 Jun 2005 08:59:06 +0900

Dear Abhilash,

Thank you for your interest on our paper. Sure you can use those figures anytime you would like to include your thesis.

Best, Younghee
Young Hee Lee, professor, Ph. D
Department of Physics
Center for Nanotubes and Nanostructured Composites
Sungkyunkwan University
Suwon, 440-746 Korea
Tel: +82-31-299-6507, 290-5954(fax)
e-mail: leeyoung@skku.edu
http://nanotube.skku.ac.kr/

----- Original Message -----  
From: Abhilash Krishna  
To: leeyoung@yurim.skku.ac.kr  
Sent: Tuesday, June 21, 2005 5:30 AM  
Subject: Permission to use figure
Dear Dr. Y. H. Lee

I am Abhilash Krishna, a master's student at Louisiana State University. My master's thesis is on Factors effecting field emission from MWNTs. For the purpose of adding in my thesis report I would like to use the figures 2 and 3 in your research paper whose details are given below.


I would really appreciate if you could grant me the permission to use your figure.

Thank you very much for your time.

Best Regards.

Abhilash Krishna

C9.

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To: "Abhilash Krishna" <akrish2@lsu.edu>
Subject: RE: Permission to use figure
Date: Tue, 21 Jun 2005 01:37:04 -0500

You can cite the reference and provide necessary description and if really necessary, then use the Fig.3 in your thesis.

Sincerely,

Sanju Gupta (Ms), Ph.D
Assistant Professor of Physics and Materials Science
SW Missouri State University
Kemper Hall, 103 M
901 South National Ave.
Springfield, MO 65804 - 0027, USA
T(O): +1-417-836-8565
F: +1-417-836-6226
E-mail: sxg535f@smsu.edu
Web mail: sgup@rocketmail.com
Webpage: http://physics.smsu.edu/faculty/Gupta/research.htm

C10.

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Proper credit must be given to our publication.

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--------Original Message from akrish2@lsu.edu---------------------------

Dear Mr. Duncan James

I am Abhilash Krishna, a master's student at Louisiana State University. My master's thesis is on Factors effecting field emission from MWNTs. For the purpose of adding in my thesis report I would like to use the figure 2(a) in the journal publication whose details are given below.


I will not be making more than 3 copies of my thesis report. I would really appreciate if you could grant me the permission to use this figure in my report.
Thank you very much for your time.
Best Regards.
Abhilash Krishna

C11.

From: "operator " operator@HUNTVAC.com
To: "Abhilash Krishna" <akrish2@lsu.edu>
CC: "Jack Crummey" <JCRummey@HUNTVAC.com>
Subject: RE: Permission to use picture
Date: Mon, 20 Jun 2005 16:45:17 -0700

Hello Sir,

We would be happy to allow use of the pictures on our website for your project. What we ask is that you accredit our facility wherever these pictures will be used. If you have any other questions please feel free to contact me.

Best Regards,

Alicia Smurphat
Customer Service Manager
Huntington Mechanical Labs
Tel: (650) 964-3323 x10
Fax: (650) 964-6153
Email: operator@huntvac.com

-----Original Message-----
From: Abhilash Krishna [mailto:akrish2@lsu.edu]
Sent: Monday, June 20, 2005 2:28 PM
To: operator
Subject: Permission to use picture

Dear Madam,

I am Abhilash Krishna, a master's student at Louisiana State University. My master's thesis is on Factors effecting field emission from MWNTs.

For the purpose of adding in my thesis report, I would like to use the picture of the Linear motion feedthrough L2141 series found on your company website mentioned below.

http://209.238.89.157/series.asp?series=L-2141

I would really appreciate if you could grant me the permission to use your figure.

Thank you very much for your time.

Best Regards.
Abhilash Krishna

C.12.

From: "Kees Hagen" C.W.Hagen@tnw.tudelft.nl
To: akrish2@lsu.edu
CC:
Subject: Copyright figures
Date: Tue, 12 Jul 2005 10:24:03 +0200

Dear Abhilash Krishna,

thank you for your interest in our work, and yes, you can use the figures in your thesis, provided you mention the source. I would appreciate it to receive a copy of your thesis when it is finished. Good luck with finishing the thesis.

Best regards,

Kees Hagen

Dr. Cornelis W. Hagen
Senior scientist
Delft University of Technology
Department of Applied Physics
Particle Optics Group
Lorentzweg 1, 2628 CJ Delft, The Netherlands
Phone: ++31-15-2786073
Fax: ++31-15-2783760
E-mail: c.w.hagen@tnw.tudelft.nl

Dear Dr. C.W. Hagen

I am Abhilash Krishna, a master's student at Louisiana State University. My master's thesis is on Factors effecting field emission from MWNTs. For the purpose of adding in my thesis report I would like to use the figure 1 & 2 in your work whose details are given below.


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Thank you very much for your time.

Best Regards.
Abhilash Krishna
Dear Mr Krishna

DIAMOND AND RELATED MATERIALS, Vol 12, No 1, 2003, Pages 422-428, Milne et al, ‘Electrical and …’, 1 Figure only

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Helen Gainford (Rights Manager)
VITA

The author, Abhilash Krishna was born in December 1980, in Andhra Pradesh, India. He graduated from Little Flower Junior College, Hyderabad, in 1998. In September 1998, the author attended Jawaharlal Nehru Technological University, Hyderabad, India, with a major in electronics and communications engineering. He obtained a Bachelor of Technology degree in electronics and communications engineering in May 2002. He continued his graduate study in electrical and computer engineering at Louisiana State University where he is currently a candidate for the degree of Master of Science in Electrical Engineering.